CONSOLIDATED TIN MINES LIMITED

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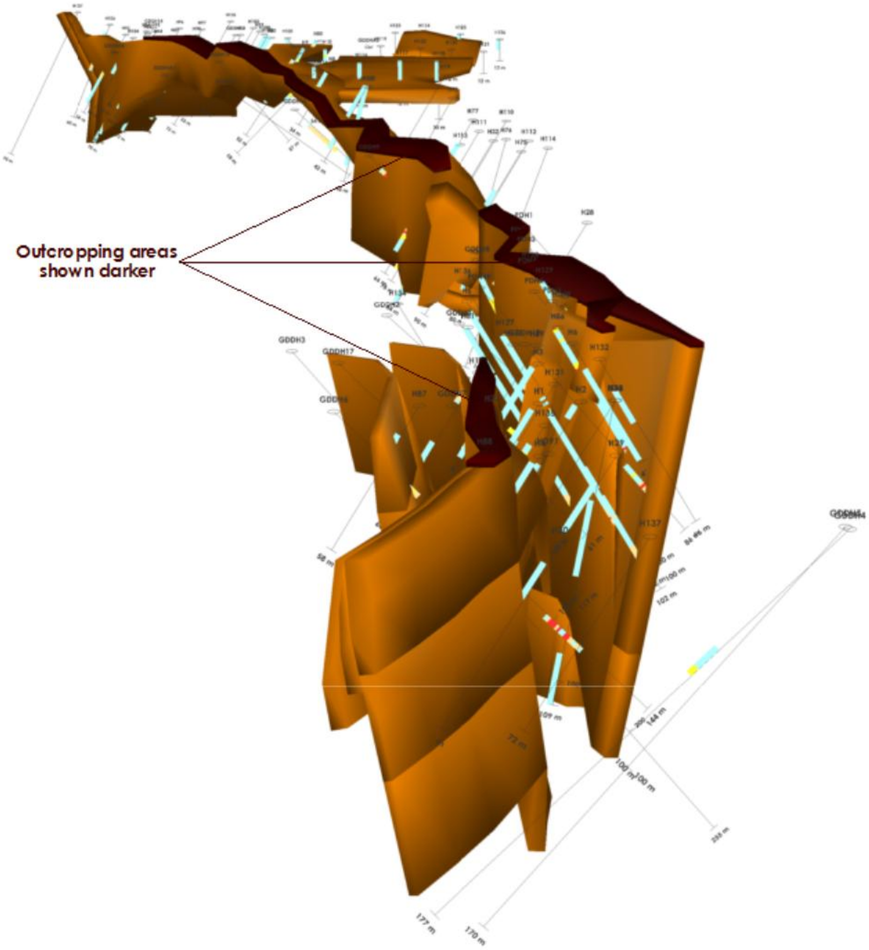
MT GARNET TIN SKARN METALLURY

EXECUTIVE SUMMARY
JUNE 2010



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FOREWORD

Consolidated Tin Mines Limited (CSD or the Company) will soon release a Scoping Study which will set the theme for future financial modelling for the development of a medium to large scale tin mining operation at the Mt Garnet area, north Queensland, Australia.

The company has complied several technical reports that explain the history and events leading to this point. These complete reports are available on the Company web site www.csdtin.com.au under the heading Investor Information/ Metallurgy.

This Executive Summary is intended to condense and summarise these Reports.

MT GARNET TIN SKARN MINERALISATION

The Mt Garnet outcropping basement geology is deformed Silurian aged limestone and carbonate sediment, sandstones, conglomerates and shales, of the Chillagoe Formation. There has been extensive Carboniferous aged granite intrusion into the Chillagoe Formation, and remaining exposures of the Chillagoe Formation are disrupted and occur as remnant sediment rafts surrounded by and eventually underplated by granite. The deformation of the Chillagoe Formation has caused the originally flat lying sediment to be upturned into steeply dipping sediment bands, including the limestone bands.

The Carboniferous granite intrusions are the causative bodies of mineral deposits not only in the Mt Garnet area but throughout the Cairns hinterland area. In the Mt Garnet area, the granites are particularly associated with tin, as the tin oxide cassiterite, mineralisation. Historically the tin mineralisation has been mined both from the granite as well as the intruded Chillagoe Formation. The Herberton Tinfield has recorded approximately 150,000 tonne of cassiterite concentrate, containing 90,000 tonne of contained tin metal, since first mining in 1880. (Note: A significant amount of tin would have gone unrecorded).

The contact of limestone and mineralising granite is a well-known geological occurrence in ore forming processes. The limestone acts as a neutralising agent for hot, acid mineralising fluids derived from the granite. Iron is generally an abundant element in and mobilised in the fluids, and the reaction of limestone and mineralising fluid causes a very significant alteration and element exchange between granite and limestone. The resulting altered rock is generally called a skarn, with that alteration generally observed as a massive magnetite replacement of the limestone. Tin and other elements in the fluid will also be deposited in the altering limestone. Due to the very strong reaction of limestone and mineralised fluid, limestones have real potential to host significant mineralisation - the fluid will dump a large volume of its minerals into a small amount of limestone.

There are only limited occurrences of limestone of the Chillagoe Formation in the Mt Garnet area. Because of the extensive granite emplacement, all the Chillagoe Formation occurrences have, to varying extents, been altered to skarns. Consolidated Tin Mines Ltd holds the known tin skarns, These skarns are outcropping as massive to semi massive iron oxide exposures (magnetite/haematite/goethite) and have the strike and dip continuity of the replaced limestone. The former precusor limestones were generally tabular, sheet type sediment bands, so the skarn rock, is a tabular sheet type band.

Consolidated Tin Mines Ltd has explored three outcropping skarns deposits, Gillian, Pinnacles and Windermere. The combined exposed strike extent for the three is 6 kilometres. True width is from 4 to 20 metres. Depth has not been closed in any of the three deposits, as the Company has concentrated its efforts to estimate the open pittable, near surface (to 80 metres vertical depth) tin mineralisation. The Company exploration has highlighted that each skarn is quite uniform in its tin mineralisation, although tin grade does vary from an average 0.8% Sn for Gillian, 0.6% Sn for Windermere and 0.4%Sn for Pinnacles.

The reaction that has produced the skarn alteration and tin mineralisation has resulted in the largest contained tin deposits in the Herberton Tinfield. The Gillian prospect on which the company has completed most exploration has a JORC compliant, contained tin content of 24,000 tonne of tin metal (3Mt at averege.8% Sn). The Company believes that within the three mentioned skarn prospects that 50,000 tonne of contained tin metal can be established.

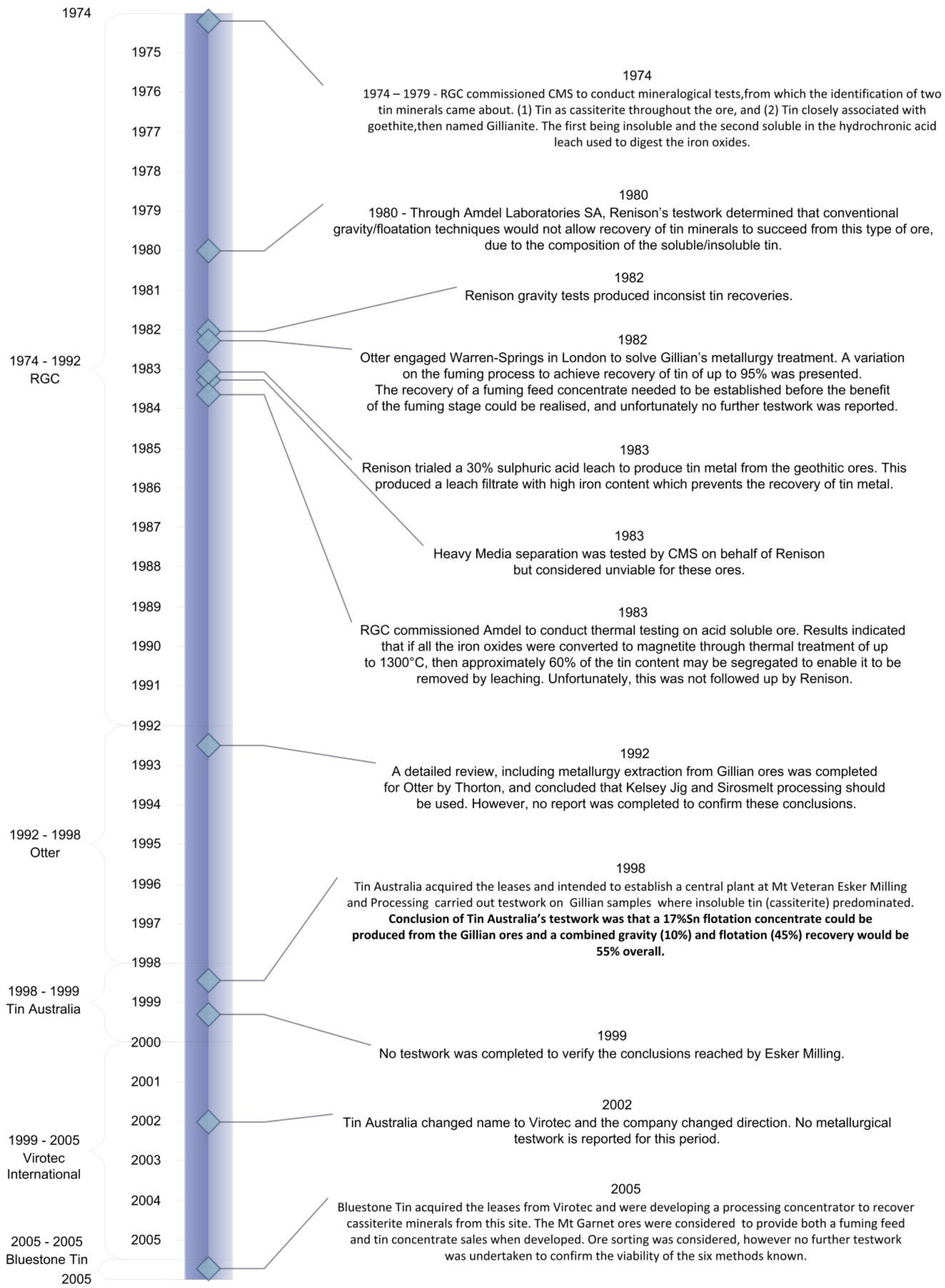
The Company also believes, based on airborne magnetic surveys it has flown and drilling evidence from historic exploration within current Company held tenements, that there are skarns that are not outcropping , but at reasonably shallow depth (from 20 metres vertical depth). The Company believes there is significant potential for ongoing tin mineralised skarn exploration success within its tenements.

Condensed from a Report by John Sainsbury - Senior Geologist & Technical Director, Consolidated Tin Mines Limited.

The ***full report*** is available on the Company web site www.csdtin.com.au under Investor information/ Metallurgy.

HISTORICAL METALLURGY TESTWORK ON MT GARNET SKARN DEPOSITS

Historical Metallurgy developments at the Mt Garnet Tin Ore deposits are represented in the following timeline.



The Gillian deposit was explored in the early 1970s by Toledo Minerals Ltd and subsequently by Otter Exploration NL and Renison Goldfields Ltd through the mid to late 1970s. Toledo completed percussion and diamond drilling, principally for base metal mineralisation, and Renison completed a 16 hole diamond drill tin exploration program. Most metallurgical work up to 2007 was done during RGC's ownership of the leases. Testing focussed on the recovery of an acid soluble tin highlighted in Renison assay work but no final conclusions regarding the viability of recovery of this tin were published.

Later, in the late 1990s, Esker Milling & Processing completed testwork of superpanning to recover the free cassiterite and up to a 38%Sn concentrate was achieved. Unfortunately, no testing was undertaken using commercially available gravity equipment, such as spirals or tables.

In brief, no assessment of a viable tin recovery as cassiterite concentrates, tin oxide fume or tin metal had been evaluated up to this point.

CONSOLIDATED TIN MINES METALLURGICAL TESTWORK & OUTCOMES

Since 2008, Consolidated Tin Mines Limited has proceeded to evaluate recovery of the tin by a commercially viable route. Particular investigation was for fine sized tin recovery with the use of centrifugal jigs. The efforts have focused on the development of a viable process to recover both marketable cassiterite at a grade suitable for conventional tin smelter operations and a lower grade tin concentrate of 10-20%Sn grade suitable for sale to a commercial tin fuming facility. The skarn deposits were also likely to be able to produce a high grade magnetite mineral for sale.

Initial Consolidated Tin Mines metallurgy investigation was undertaken by Esker Milling and Processing Pty Ltd, by experienced tin metallurgist Nick Moony. The testwork, on a composite drill sample from a Gillian drill Hole 7, reported that a tin recovery of 30% was achieved when producing a 50%Sn concentrate; at a 17-22%Sn concentrate the tin recovery rose to 50-55% and another 15-20% recovery could be achieved into a 4.5%Sn low grade concentrate. The recovery of iron from this ore was estimated at 50% at an iron concentrate grade of 65%. The testing used Low Intensity Magnetic Separation (LIMS) and Wet High Intensity Magnetic Separation (WHIMS) at a range of magnetic flux densities. The Esker work showed promise in extraction of a saleable tin concentrate exceeding 50%Sn content but at only 30% recovery. It was summarised that a further 30-40% of the tin could be recovered to a 6-12%Sn grade. Esker recommended that tin flotation testing needed to be optimized. The use of enhanced gravity methods also needed to be investigated in order to achieve optimal recovery of the free cassiterite.

From August 2009, the Company has employed experienced tin metallurgist, Mr. Robert Shelley. The testwork was directed to investigate and improve the earlier results. An immediate requirement was establishment of the grind size for liberation of cassiterite from the predominantly iron oxide gangue (the iron oxides being magnetite, haematite and goethite). Ongoing testwork then involved the best commercial recovery methods for the liberated cassiterite, as well as the liberated iron oxides.

First testwork involved QEMSCAN (Electron Microscope) examination of ground samples to outline cassiterite liberation. Two samples were chosen, one sample from Gillian Hole 7 was considered to contain a coarser cassiterite, and the second sample, from a composite of Gillian Holes 83 and 84, which was considered to contain a greater component of fine cassiterite. A component of each sample was ground to 106 microns. For Hole 7, average grain size of the cassiterite particles was 13.27 microns and the QEMSCAN indicated that 73% of cassiterite particles were over10 microns with the remainder 27% at 7 to10 microns. Only cassiterite was identified in the sample with no stanniferrous goethite detected. For Hole 83/84 average grain size of the cassiterite particles found in the sample was 10.09 microns. In this case 50% was above10 microns, 29% at 7 to10 microns, 13% at 5 to7 microns and 8% at less than 5 microns. Only cassiterite was identified in this sample.

The QEMSCAN examination highlighted that cassiterite was at a size considered to be close to the limit of the size range for cassiterite recovery, but recovery should be achieved with well understood recovery processing and with commercially available equipment. The sizing also highlighted that the cassiterite would be optimally recovered into two concentrates - a gravity circuit concentrate and a flotation circuit concentrate. The testwork was to maximise the cassiterite reporting to the gravity circuit, where the high density of cassiterite could be utilised in the concentration process. The QEMSCAN analyses confirmed that the cassiterite was closely associated with iron oxides, and that separation of the oxides by magnetic separation was going to be essential as the first step in producing saleable tin concentrate grades.

Testwork continues to achieve optimal recoveries; what the testwork to date has suggested is a crushing and grinding circuit to achieve a p80 (80%) at around 50 microns.

The first stage of processing will be LIMS (Low Intensity Magnetic Separation) Separation. This step removes a lot of heavy magnetite from the circuit, with minimal loss of tin and production of a high grade iron concentrate. A field strength of 1300 gauss is suggested with the magnetite/martite product of iron grade of 68% Fe and tin grade of 0.25%Sn (10% loss of tin from the feed).

The LIMS Non Magnetic product is subject to classification with the plus 10 micron product to be subjected to enhanced gravity separation using Kelsey jigs to produce a concentrate which will then be upgraded to plus 40%Sn concentrate using Holman fine roughing and cleaning tables.

A portion of the tailings from the gravity treatment circuit are then returned to the circuit and this is inert media ground to 10 micron sizing. This product is processed through an Outotec SLon type HIM (High Intensity Magnetic) separator, which will produce magnetic product with high hematite content and a non magnetic product. The HIMS (SLon) circuit will require a roughing stage and cleaning stage for the magnetic stream, and a scavenging stage for the non magnetic stream. This configuration will ensure that both magnetic and non magnetic products are as clean as possible for further treatment. The non magnetic product has a reduced level of hematite and high goethite content but contains free cassiterite which is recoverable by tin flotation directly or may require acid dissolution treatment or enhanced gravity treatment (UF Falcon) in order to complete the liberation of free cassiterite and removal of ultrafine slimes. The goal for the SLon non magnetic product is to achieve maximum recovery of tin to a flotation product of 10-20%Sn grade.

The LIMS magnetic product, the SLon magnetic product and the table middling's will be treated by tin fuming at 1250°C. This method will give the highest recovery of tin to an oxide fume and a grade exceeding 70%Sn content.

Testwork to date has a projected recovery value of 68% which is commercially viable, with improvements in the ongoing programs expected to increase this to 70/75% recovery.

Condensed from a Report by Robert Shelley - Senior Development Metallurgist, Consolidated Tin Mines Limited. The full Report is available on www.csdtin.com.au under Investor Information/ Metallurgy.

Also note that this Report has been reviewed by independent Senior Consulting Metallurgist Ron Goodman. Ron has extensive experience in this field and has been involved with the Mt Garnet Skarn ores in the past (prior to CSD involvement).
Ron Goodman's Review is also available at www.csdtin.com.au under investor Information/ Metallurgy.

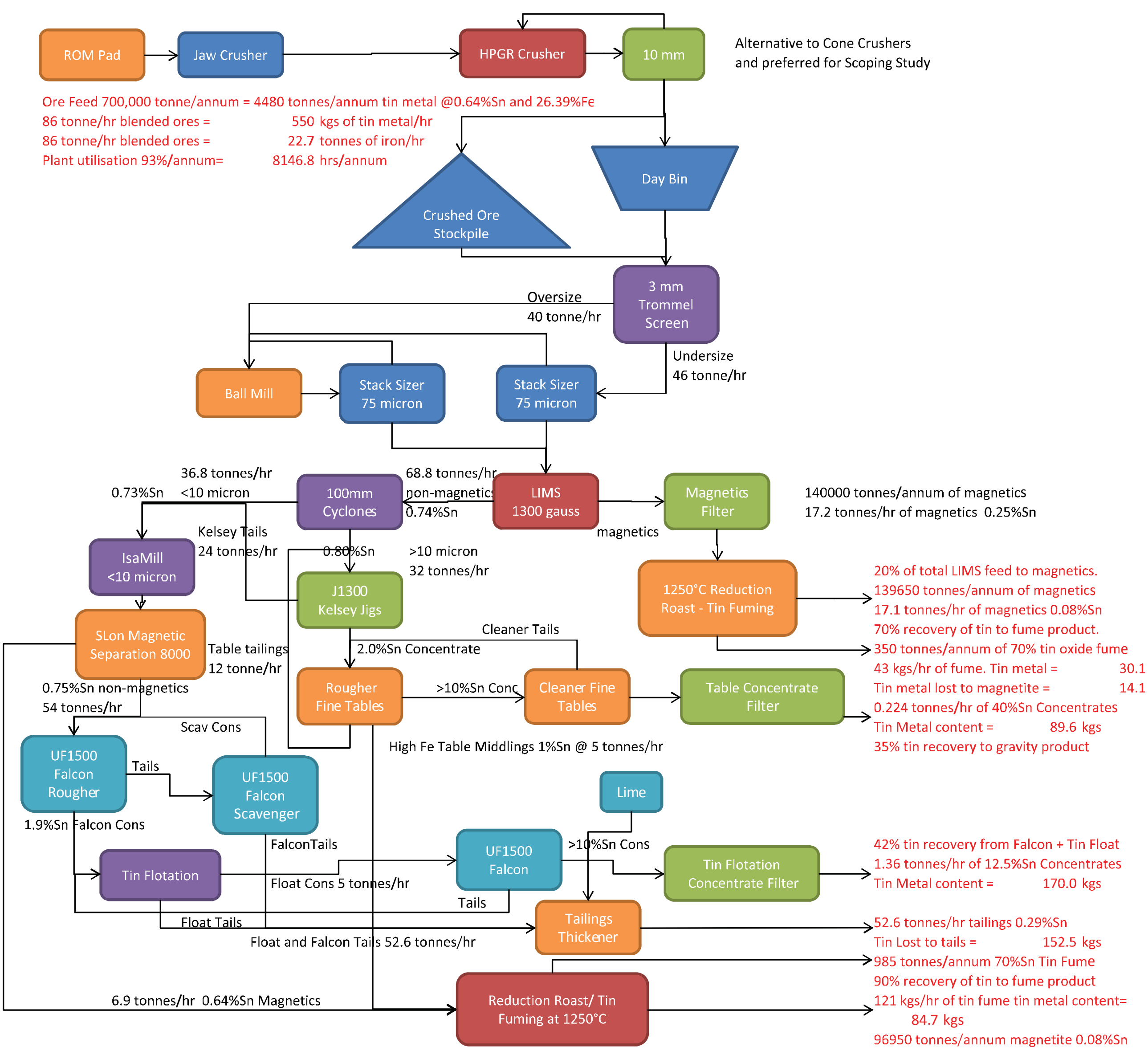
MT GARNET FLOW SHEET

This flow sheet has been developed by Robert Shelley -Senior Development Metallurgist, Consolidated Tin Mines Limited and Reviewed by SEMF Pty Ltd, Independent consultants to CSD.

SEMF has over thirty years experience in heavy mining and bulk handling products of this nature. In particular SEMF has performed similar work for BHP, Rio Tinto, Comalco Mining and Refining, MM Kembla and others .SEMF has particular experience in tin mining at Renison Bell in Tasmania. A current project for King Island Scheelite involves a metallurgy process that is likely to be similar to CSD.

The fully documented Report prepared by SEMF is also available at www.csdtin.com.au under Investor information/Metallurgy

Proposed Flowsheet for Treatment of Mt Garnet Ores- June 2010



Total kgs/hr of contained tin metal products =	374.4 kgs	
Total Recovery to saleable tin products =	68.02 % from hourly products	
Tin metal kgs/hr losses =	174.4	
Tin Fume product at 70%Sn grade =	1335 tonnes/annum =	935 tonnes of tin content/annum
Gravity tin concentrate at 40%Sn grade =	1825 tonnes/annum =	730 tonnes of tin content/annum
Flotation tin concentrate at 12.5%Sn =	11080 tonnes/annum =	1385 tonnes of tin content/annum
Total tin content of all products =		3049 tonnes of tin content/annum
Total recovery of tin metal from annual products =		68.07 %
Total tonnage of roasted magnetite mineral products of >65%Fe content		236600 tonnes /annum

ENDS

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The information contained in this report that relates to assay results of rock samples and drill chips, to mineral resource estimates and to ore reserve estimates of mineralisation is based on information compiled by John Sainsbury (BSc, AusIMM) an executive director of Consolidated Tin Mines Limited. John Sainsbury is a geologist of 30 years experience and has sufficient experience in the type of mineralisation under consideration to qualify as a Competent Person as defined by the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves - JORC Code, 2004 Edition. John Sainsbury has consented to the inclusion of this information in the form and context in which it appears.

ABOUT CONSOLIDATED TIN MINES LIMITED

The Company's goal is to become Queensland's premier tin producing company. Consolidated Tin's short to medium term goals are:

- To further expand resources across its three key projects; Gillian, Pinnacles and Windermere to identify 8 to 10Mt JORC Resource
- Develop a hard rock mining operation
- Develop a centrally located mill capable of 1Mtpa
- Develop an alluvial mining operation
- Explore other known mineralisation in current tenement holding to provide resource expansion and additional mine life.